

Exercise 5.6

From Figure 5.24 at an operating point defined by  $V_{GSQ} = 2.5$  V and  $V_{DSQ} = 6$  V, we have

$$g_m = \frac{\Delta i_D}{\Delta v_{GS}} = \frac{(4.4 - 1.1) \text{ mA}}{1 \text{ V}} = 3.3 \text{ mS}$$

$$1/r_d = \frac{\Delta i_D}{\Delta v_{DS}} \cong \frac{(2.9 - 2.3) \text{ mA}}{(14 - 2) \text{ V}} = 0.05 \times 10^{-3}$$

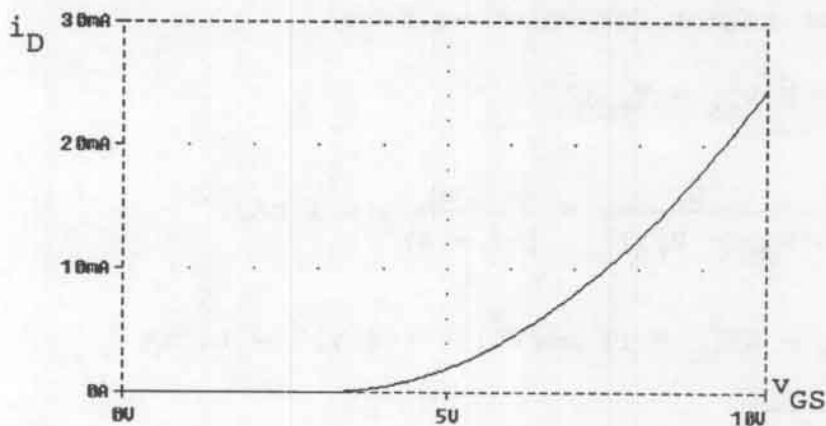
Taking the reciprocal, we find  $r_d = 20 \text{ k}\Omega$

Exercise 5.7

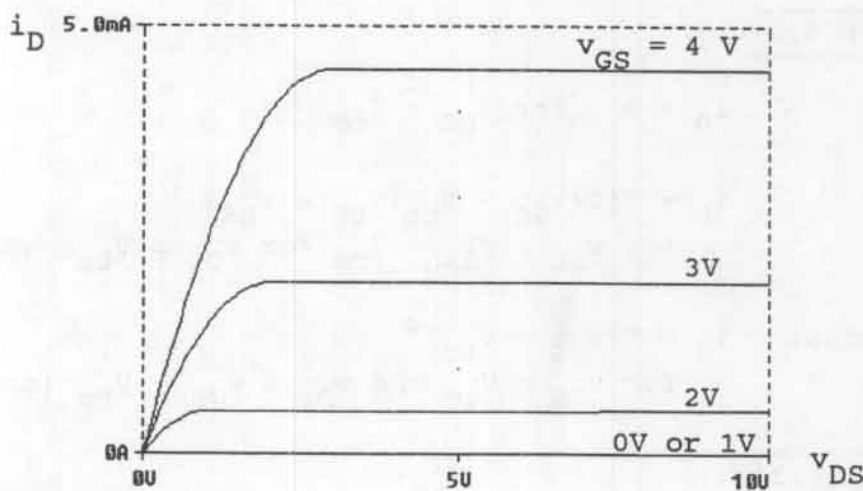
$$\begin{aligned}g_m &= \left. \frac{\partial i_D}{\partial v_{GS}} \right|_{\text{Q-point}} \\&= \left. \frac{\partial}{\partial v_{GS}} K(v_{GS} - v_{to})^2 \right|_{\text{Q-point}} \\&= 2K(v_{GSQ} - v_{to})\end{aligned}$$

Problem 5.4

The device is in saturation for  $v_{DS} \geq v_{GS} - V_{to} = 2 \text{ V}$ . The device is in the triode region for  $v_{DS} \leq 2 \text{ V}$ . The plot of  $i_D$  versus  $v_{GS}$  in the saturation region is:



Problem 5.5



Problem 5.6

(a) Cutoff because we have  $v_{GS} \leq V_{to}$ .

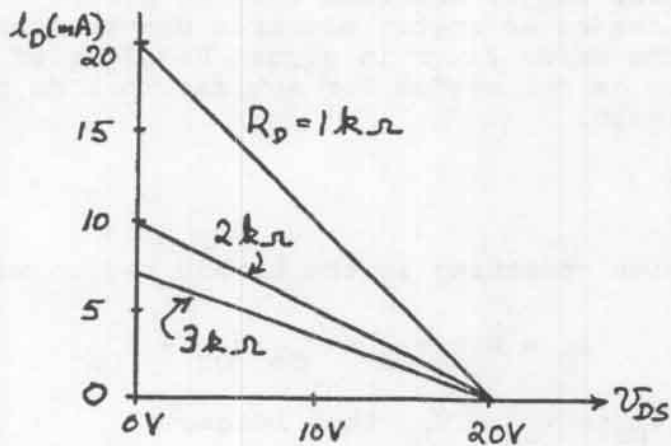
(b) Triode because we have  $v_{DS} < v_{GS} - V_{to}$  and  $v_{GS} \geq V_{to}$ .

(c) Saturation because we have  $v_{GS} \geq V_{to}$  and  $v_{DS} \geq v_{GS} - V_{to}$ .

(d) Saturation because we have  $v_{GS} \geq V_{to}$  and  $v_{DS} \geq v_{GS} - V_{to}$ .

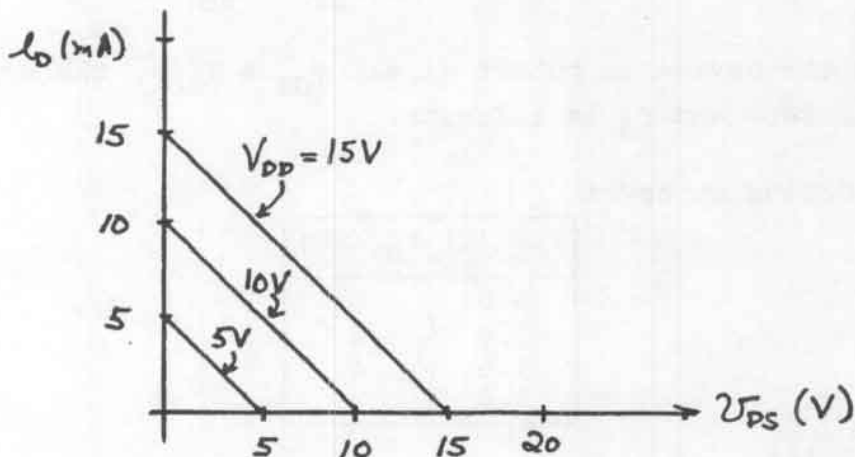
Problem 5.15

The load-line equation is  $V_{DD} = R_D i_D + v_{DS}$ , and the plots are shown on the next page.



Notice that the load line rotates around the point  $(V_{DD}, 0)$  as the resistance changes.

Problem 5.16



Notice that the load lines are parallel as long as  $R_D$  is constant.

Problem 5.22

For this circuit we can write

$$V_{GSQ} = 15 - I_{DQ}R_S$$

Assuming operation in saturation, we have

$$I_{DQ} = K(V_{GSQ} - V_{to})^2$$

using the first equation to substitute into the second equation we have

$$I_{DQ} = K(15 - I_{DQ}R_S - V_{to})^2 = 0.25(14 - 3I_{DQ})^2$$

where we have assumed that  $I_{DQ}$  is in mA. Rearranging we have

$$I_{DQ}^2 - 9.777I_{DQ} + 21.777 = 0$$

The correct root is the smaller one which is  $I_{DQ} = 3.432$  mA. Then we have  $V_{DSQ} = 30 - R_D I_{DQ} - R_S I_{DQ} = 16.27$  V.

**Problem 5.23**

Assuming that the MOSFET is in saturation, we have

$$V_{GSQ} = 10 - I_{DQ}$$
$$I_{DQ} = K(V_{GSQ} - V_{to})^2$$

where we have assumed that  $I_{DQ}$  and  $K$  are in mA and mA/V<sup>2</sup> respectively.

(a) Using the second equation to substitute in the first, substituting values and rearranging, we have

$$V_{GSQ}^2 - 7V_{GSQ} + 6 = 0$$

which yields

$$V_{GSQ} = 6 \text{ V}$$

(The other root,  $V_{GSQ} = 1$  V, is extraneous.)

$$I_{DQ} = 4 \text{ mA}$$

$$V_{DSQ} = 10 - 2I_{DQ} = 12 \text{ V}$$

(b) Similarly we have

$$V_{GSQ}^2 - 3.5V_{GSQ} - 1 = 0$$

$$V_{GSQ} = 3.765 \text{ V}$$

$$I_{DQ} = 6.234 \text{ mA}$$

$$V_{DSQ} = 20 - 2I_{DQ} = 7.53$$

Problem 5.27

We have  $V_{GSQ} = V_{DSQ} = V_{DD} - R_D I_{DQ}$ . Then substituting  $I_{DQ} = K(V_{GSQ} - V_{to})^2$ , we have

$$V_{GSQ} = V_{DD} - R_D K (V_{GSQ} - V_{to})^2$$

Substituting values and rearranging, we have

$$V_{GSQ}^2 + 2V_{GSQ} - 39 = 0$$

Solving we determine that  $V_{GSQ} = 5.325$  V and then we have  $I_{DQ} = K(V_{GSQ} - V_{to})^2 = 4.675$  mA.